

BROADBAND

RESONANT MASS

GW DETECTOR

The "DUAL SPHERE"

concept: NOT (yet)

a feasibility study

attractive:

sensitive @ high frequencies (kHz)

complementary to "advanced" ifo

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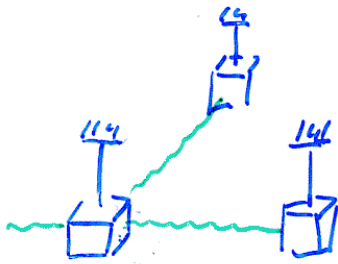
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OPTOMECHANICAL

G.W. DETECTORS



km BASELINE
INTERFEROMETERS

"WIDE" BAND
 $\Delta f \sim f$



CRYOGENIC RESONANT BARS
WITH RESONANT OPTOMECHANICAL
TRANSDUCER

"NARROW" BAND $\Delta f \approx 0.1 f$

a third possibility:

NON RESONANT OPTICAL READOUT + MASSIVE RESONANT SPHERES

CONCENTRIC
FULL + HOLLOW SPHERE

{ sapphire, YAG, Si } ~ 3m
30 t + 30 t

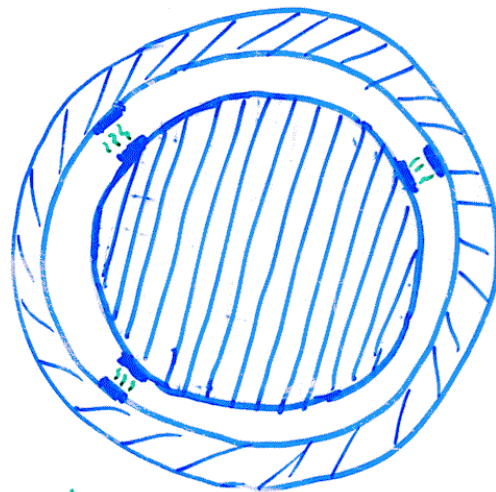
FABRY-PEROT CAVITIES

low losses 1 ppm
high finesse 3×10^5
high laser power 1 W

$$S_{\frac{1}{2}}(f) \approx 1 \times 10^{-23} \text{ Hz}^{-1/2}$$

$$1000 \text{ Hz} \leq f \leq 3000 \text{ Hz}$$

↳ "WIDE" BAND



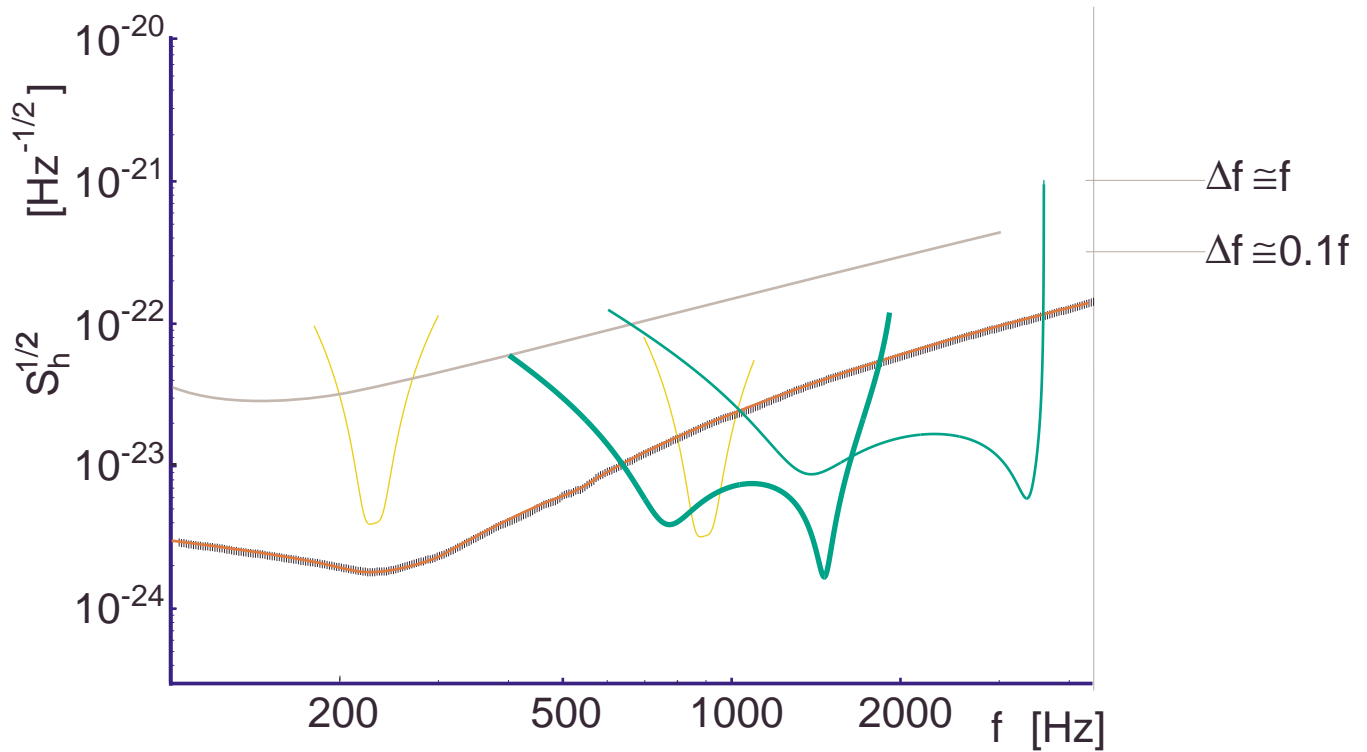
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_____ LIGO I , VIRGO

_____ LIGO II

_____ CuAl^{10%} hollow sphere 4.4 m diameter
resonant transducer and SQL

sapphire “dual spheres” $Q/T \sim 5 \cdot 10^8 \text{ K}^{-1}$ and SQL
FP cavities: 2 cm $F \sim 10^6$

_____ 100 t + 100 t 4.6 m diameter $P_{in} \sim 3 \text{ W}$

_____ 30 t + 8 t 2.3 m diameter $P_{in} \sim 8 \text{ W}$



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resonant mass gu detectors are quoted

as "INTRINSICALLY NARROW BAND"

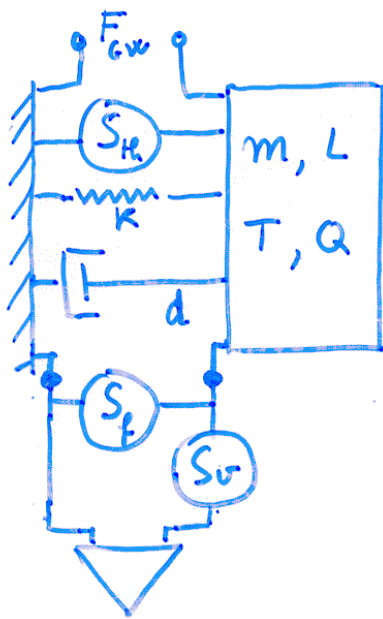
are they? NO! ←

↳ YES IN PRACTICE

multimode $n \geq 3 \Rightarrow \Delta f \sim f$

BUT in operation until max $n=2 \Rightarrow \Delta f < 0.1 f$

a "ONE MODE" detector PRICE PRD36 (87)



res. mass

$$\omega_0 = \sqrt{\frac{k}{m}} \quad d = \frac{\omega_0 m}{Q}$$

$$F_{GW}(\omega) = \frac{2}{\pi^2} m L \omega^2 h(\omega)$$

$$S_H(\omega) = 2 k_B T d$$

mech. amplifier

$$S_v(\omega) = \omega^2 S_x(\omega) \quad \leftarrow \text{displ. noise}$$

$$S_f(\omega) \rightarrow \text{"back action"}$$

$$\sqrt{S_f S_v} = k_B T_n \quad \sqrt{\frac{S_f}{S_v}} = z_m$$

$$S_f = k_B T_n z_m$$

best performance:
 "LOSSLESS LIMIT" $S_{H_e}(\omega) \ll S_f(\omega) \Rightarrow Q \gg \frac{2T}{T_n} \frac{\omega_0 m}{z_m}$
 $\hookrightarrow \frac{\Delta f}{f} = \frac{z_m}{\omega_0 m}$ $\left\{ \text{SQL} \Rightarrow T_n \approx \frac{1}{2} \omega_0 \right\}$

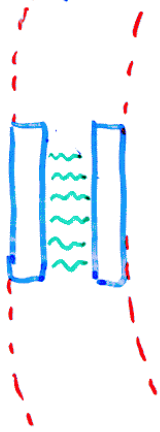
at the time (SQUIDS) $\frac{z_m}{\omega_0 m} \approx 10^{-5} - 10^{-7}$



NON-resonant optomechanical transducers

reading motion of RESONANT mass(es)

↳ (mechanically non-resonant) version of: CONTI et al RSI 69 (98)



Fabry-Pérot cavity

"short" ~ 1 cm

low loss ~ 1 ppm

high finesse $\mathcal{F} \approx 10^6$

high input power $P \approx 10$ W

$$\mathcal{Z}_m \equiv \sqrt{\frac{S_t}{\omega^2 S_x}} \approx B \frac{\mathcal{F}^2 P}{\omega_0}$$

$$B(\chi_{\text{cav}}, \eta, A_{\text{mod}}) \approx 4 \times 10^{-3} \text{ } \mu\text{m}^2, \quad m \sim \text{tons}, \quad \frac{\omega_0}{2\pi} \sim \text{kHz}$$

$$\frac{\Delta f}{f} \equiv \frac{\mathcal{Z}_m}{\omega_0 m} \approx 0.1$$

suggest that the bandwidth
can be much BROADER !



- each F-P cavity mirror part of a low thermal noise mechanical system \Rightarrow DUAL SPHERE
- "omnidirectional" sensitivity \Rightarrow 6 cavities (TIGA)
5 " (Lobo)
sense RADIAL displ.
- readout SQL: $\frac{k_B T}{Q} \approx \hbar \Delta f \Rightarrow \Delta f \approx \frac{Q}{T} \approx 10^8 \text{ K}^{-1}$
- large "cross section" $\sim g \nu_s^5 \Rightarrow \text{CuAl}^{10\%}, \text{YAG}, \text{Si SAPPHIRE}$

RADIAL DISPLACEMENT $x(\omega) \propto \omega^2 \tilde{h}(\omega)$

- write: $S_x(\omega)$ as due to thermal + back-action and to ALL modes (also those non-gu sensitive)
- $\begin{matrix} \text{hollow} & \downarrow & \text{full} \\ \omega_{me} & , & \omega_{me} \end{matrix}$

- find:

$$S_h(\omega) = \frac{S_{x, \text{hollow}}^{\text{th+ba}}(\omega) + S_{x, \text{full}}^{\text{th+ba}}(\omega) + S_x^{\text{shot}}(\omega)}{|x_{\text{hollow}}(\omega) - x_{\text{full}}(\omega)|^2 / |\tilde{h}(\omega)|^2}$$

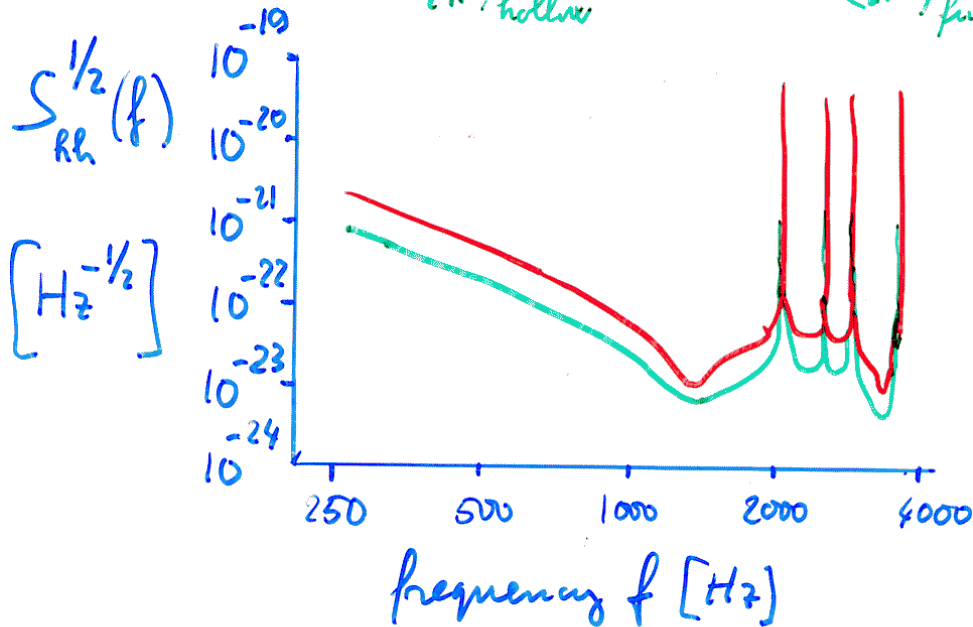
- for $\omega_{\text{hollow}} < \omega < \omega_{\text{full}}$ signals ADD
- for some $\omega^* > \omega_{\text{hollow}}, \omega_{\text{full}}$ signal CANCEL



Sapphire 2.6 m o.d. 30+8 tons

"DUAL SPHERE" spectral strain noise

$$\left(\frac{\omega_0}{2\pi}\right)_{\text{hollow}} = 1300 \text{ Hz} \quad \left(\frac{\omega_0}{2\pi}\right)_{\text{full}} = 3370 \text{ Hz}$$



- "light" SQL @ 1500 Hz $\frac{Q}{T} = 5 \times 10^8 \text{ K}^{-1}$ $P = 8 \text{ W}$
- thermal + shot noise regime $\frac{Q}{T} = 10^8 \text{ K}^{-1}$ $P = 1 \text{ W}$

notice

- few NON-GW active resonances \rightarrow thermal noise
- $1300 \text{ Hz} < f < 3370 \text{ Hz}$ signal drives hollow sphere ABOVE resonance and full sphere BELOW resonance \rightarrow DIFFERENTIAL MOTION TRANSDUCER READS SUM OF RESPONSES
- $f \sim 4000 \text{ Hz} \rightarrow$ RESPONSES CANCEL OUT



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before an actual feasibility study:

show stoppers ???

• FABRICATION

CuAl^{10%}

YAG, Si, Al₂O₃ silicate, SAB bonded

preserving $Q \approx 10^8$

• CRYOGENICS

cool to $T \sim 1K$

and drag out few watts

• SUSPENSIONS

$m \approx 10^+$

"freely" one sphere in respect to the other

• CRYOPTICS

F-P cavities demonstrated at low T

but at lower F and much lower P



• THERMOELASTIC NOISE

OK

.....?

coating th. noise?

